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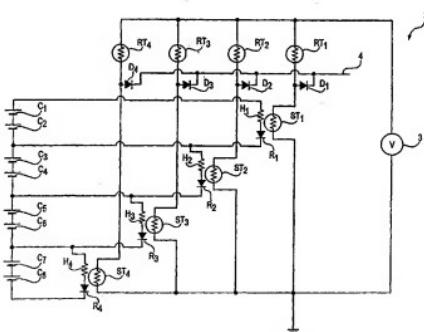
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(54) Title: CELL VOLTAGE MONITOR FOR A FUEL CELL STACK



(57) Abstract: Voltage reversal in fuel cell stacks may be detected and/or prevented by monitoring each cell or small groups of cells in the stack for low voltage conditions. An improved cell voltage monitor is constructed using a plurality of voltage monitoring units in which each unit comprises a heating resistor, a rectifier in series therewith, and a sensing thermistor in thermal communication with the heating resistor. The heating resistor is electrically connected across a cell or cells and heats the associated sensing thermistor in accordance with the voltage of the cell(s). Since the resistance of the sensing thermistor is indicative of its temperature and hence also of voltage of the cell(s), the sensing thermistor resistance can be used to signal a low voltage condition.

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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

CELL VOLTAGE MONITOR FOR A FUEL CELL STACK

Field of the Invention

The present invention relates to apparatus and
5 methods for monitoring cell voltages in fuel cell
stacks. In particular, the present invention
relates to monitoring cell voltages for purposes of
detecting and preventing voltage reversal conditions
in solid polymer electrolyte fuel cells.

10

Background of the Invention

Fuel cell systems are currently being developed
for use as power supplies in numerous applications,
such as automobiles and stationary power plants.
15 Such systems offer promise of economically
delivering power with environmental and other
benefits. To be commercially viable however, fuel
cell systems need to exhibit adequate reliability in
operation, even when the fuel cells are subjected to
20 conditions outside the preferred operating range.

Fuel cells convert reactants, namely fuel and
oxidant, to generate electric power and reaction
products. Fuel cells generally employ an
electrolyte disposed between two electrodes, namely
25 a cathode and an anode. A catalyst typically
induces the desired electrochemical reactions at the
electrodes. Preferred fuel cell types include solid
polymer electrolyte fuel cells that comprise a solid
polymer electrolyte and operate at relatively low
30 temperatures.

A broad range of reactants can be used in solid
polymer electrolyte fuel cells. For example, the
fuel stream may be substantially pure hydrogen gas,

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a gaseous hydrogen-containing reformate stream, or methanol in a direct methanol fuel cell.

The oxidant may be, for example, substantially pure oxygen or a dilute oxygen stream such as
5 air.

During normal operation of a solid polymer electrolyte fuel cell, fuel is electrochemically oxidized at the anode catalyst, typically resulting in the generation
10 of protons, electrons, and possibly other species depending on the fuel employed. The protons are conducted from the reaction sites at which they are generated, through the electrolyte, to electrochemically react with
15 the oxidant at the cathode catalyst. The catalysts are preferably located at the interfaces between each electrode and the adjacent electrolyte.

Solid polymer electrolyte fuel cells
20 employ a membrane electrode assembly ("MEA") which comprises the solid polymer electrolyte or ion-exchange membrane disposed between the two electrodes. Separator plates, or flow field plates for directing the reactants across
25 one surface of each electrode substrate, are disposed on each side of the MEA.

In operation, the output voltage of an individual fuel cell under load is generally below one volt. Therefore, in order to provide
30 greater output voltage, numerous cells are usually stacked together and are connected in series to create a higher voltage fuel cell

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stack. (End plate assemblies are placed at each end of the stack to hold it together and to compress the stack components together.

Compressive force is needed for effecting seals
5 and making adequate electrical contact between various stack components.) Fuel cell stacks can then be further connected in series and/or parallel combinations to form larger arrays for delivering higher voltages and/or currents.

10 However, fuel cells in series are potentially subject to voltage reversal, a situation where a cell is forced to the opposite polarity by the other cells in the series. This can occur when a cell is unable
15 to produce the current forced through it by the rest of the cells. Groups of cells within a stack can also undergo voltage reversal and even entire stacks can be driven into voltage reversal by other stacks in an array. Aside
20 from the loss of power associated with one or more cells going into voltage reversal, this situation poses reliability concerns.

Undesirable electrochemical reactions may occur, which may detrimentally affect fuel cell
25 components. Component degradation reduces the reliability and performance of the fuel cell.

The adverse effects of voltage reversal can be prevented, for instance, by employing rectifiers capable of carrying the stack
30 current across each individual fuel cell. Alternatively, the voltage of each individual fuel cell may be monitored and an affected

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stack shut down if a low cell voltage is detected. However, given that stacks typically employ numerous fuel cells, such approaches can be quite complex and expensive to implement.

5 The complexity and expense of cell voltage monitors can be reduced by monitoring and comparing the voltages of suitable groups of cells instead of individual cells, as disclosed in U.S. Patent No. 5,170,124. Another approach
10 is disclosed in European Patent publication number EP 982788 in which optoisolators are used to monitor voltages across pairs of cells in a stack. A photoemitter activates and illuminates a photo-detector in each
15 optoisolator when the summed voltage of the monitored pair of cells exceeds an activating voltage. The photo-detectors are connected in series and current can pass through when all the photoemitters are activated. However, a
20 low voltage condition in any pair causes the associated photoemitter to darken, opening the photo-detector, and interrupting the flow of current. The absence of current flow is detected and provides warning of potential
25 voltage reversal conditions in the stack.
There are certain disadvantages with using optoisolators however. For instance, optoisolators are yes-no devices and do not provide an indication of the severity of the
30 problem. Further, the response of an optoisolator may be fast enough that noise spikes might affect output, thereby

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necessitating signal conditioning. Most importantly, optoisolators have a specific "on" voltage (about 1.2 V) which can limit their effectiveness in this application. For 5 instance, in a stack where the normal operating cell voltage was always over 0.6 V, a pair of "normal" cells would reliably activate the optoisolator. However, if the normal operating cell voltage could be about 0.6 V or less, then 10 a pair of "normal" cells would not reliably activate the optoisolator. In addition, monitoring a three cell group could not be an acceptable option in some circumstances because a three cell group consisting of two "normal" 15 cells operating at 0.8 V and one cell undergoing voltage reversal could still activate the optoisolator.

Other approaches may also be considered in order to detect voltage reversal conditions. 20 For instance, a specially constructed sensor cell may be employed that is more sensitive than other fuel cells in the stack to certain conditions leading to voltage reversal (for example, fuel starvation of the stack). Thus, 25 instead of monitoring many cells in a stack, only the sensor cell need be monitored and used to prevent widespread cell voltage reversal under such conditions. However, other conditions leading to voltage reversal may 30 exist that a sensor cell cannot detect (for example, a defective individual cell in the stack). As another example, an exhaust gas

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monitor may be employed that detects voltage reversal by detecting the presence of or abnormal amounts of species in an exhaust gas of a fuel cell stack that originate from 5 reactions that occur during reversal. While exhaust gas monitors can detect a reversal condition occurring within any cell in a stack and they may suggest the cause of reversal, such monitors do not generally provide any 10 warning of an impending voltage reversal. Thus, voltage monitors offer certain advantages over these other approaches and may therefore be desirable for voltage reversal protection.

15

Summary of the Invention

An improved cell voltage monitor for fuel cell stacks employs voltage monitoring units for monitoring cell voltage. The voltage 20 monitoring units comprise a heating resistor, a rectifier in series with the heating resistor, and a sensing thermistor. A thermistor is a thermally sensitive resistor whose resistance varies predictably as a function of 25 temperature. The sensing thermistor is used to sense heat generated by the heating resistor and, for this purpose, is positioned to be in thermal communication with, but electrically isolated from, the heating resistor.

30 The series-connected heating resistor and rectifier in the voltage monitoring unit are electrically-connected across one or more fuel

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cells in the stack. The polarity of the rectifier is arranged such that current is prevented from flowing through the series-connected resistor and rectifier when the
5 voltage across the fuel cell or cells changes polarity during voltage reversal. During normal operation of the fuel cell stack however, the heating resistor is resistively heated by the fuel cell. The amount of heat
10 generated and communicated to the sensing thermistor is a function of the voltage across the heating resistor. Thus, the temperature and hence the resistance of the sensing thermistor are indicative of fuel cell voltage.

15 To detect a low voltage condition, a determination is made as to whether the sensing thermistor resistance is in a range associated with low cell voltage. In this regard, a signal indicative of the sensing thermistor
20 resistance can be obtained using a reference thermistor. For instance, the reference thermistor may be connected in series with the sensing thermistor but is thermally isolated therefrom. A reference voltage may then be
25 applied across the series-connected sensing and reference thermistors and the voltage across the sensing thermistor measured. The resistance of the sensing thermistor may then be determined by comparing the voltage across
30 the sensing thermistor to the reference voltage. An advantage of this approach is that the comparison can provide information about

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the extent of a low voltage condition along with the mere indication of the problem.

A preferred embodiment employs reference and sensing thermistors having the same

5 resistance versus temperature characteristics (for example, same type). A diode may also be employed to prevent other signals (for example, signals from other voltage monitoring units) from affecting the sensing thermistor voltage.

10 One end of the diode may be electrically-connected between the series-connected sensing and reference thermistors.

Resistance changes in the sensing thermistor are more readily detected if the
15 resistance changes substantially with an increase in temperature above ambient. A resettable thermal switch, such as a polymeric positive temperature coefficient (PTC) fuse, may undergo a marked increase in resistance
20 with temperature and is suitable for use as a sensing thermistor. In such an embodiment, the PTC fuse might be heated sufficiently during normal operation to be "open", but insufficiently heated during a low voltage
25 condition and be "closed". A low voltage condition might thus simply be indicated by determining if the PTC fuse was open or closed. However, this approach does not provide quantitative information about the extent of a
30 low voltage condition.

Preferably, the heating resistor in the voltage monitoring unit is also a positive

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temperature coefficient thermistor (that is, a heating thermistor) to reduce power consumption over the higher end of the normal operating voltage range of the fuel cells in the stack.

5 A cell voltage monitor for a fuel cell stack may comprise a plurality of the preceding voltage monitoring units. The series-connected heating resistors and rectifiers in each of the plurality of voltage monitoring units may
10 themselves be connected in series. The plurality of voltage monitoring units may conveniently be mounted on a flexible printed circuit board. The heating resistor, the rectifier, and the sensing thermistor in a
15 given voltage monitoring unit may be mounted closely together and coated with a suitable thermally conductive material, such as a thermosetting polymer. Other components may be mounted at a distance for purposes of thermal
20 isolation.

In an embodiment employing reference thermistors and diodes (such as that described above), the series-connected reference thermistors and sensing thermistors in each of
25 the plurality of voltage monitoring units are conveniently connected in parallel across the reference power supply. The other ends of the diodes may be connected to a common signal line and the polarity of the diodes may be set such
30 that current is prevented from flowing from an unheated sensing thermistor to any heated thermistor. In this way, when the sensing

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circuit is arranged such that an unheated sensing thermistor generates a greater signal than the heated ones, the diodes stop the greater signal from sinking through the heated 5 thermistor circuits. The presence of the greater signal on the signal line is indicative of a low voltage cell.

In an embodiment employing resettable thermal fuses (such as that described above), 10 the resettable thermal switches in each of the plurality of voltage monitoring units may be connected in parallel. An "open" circuit condition might then exist in this parallel circuit of switches when all the cells are 15 operating in a normal voltage range. However, a single low voltage cell would result in a "closed" circuit condition in one of the fuses and hence in the parallel circuit.

A voltage monitoring unit may be used to 20 monitor the voltage of one or more fuel cells (for example, a pair of cells) in a fuel cell stack by electrically-connecting the series-connected heating resistor and rectifier in the unit across the cell or cells. In order to 25 monitor the voltages of all the series-connected fuel cells in a fuel cell stack, generally a cell voltage monitor would be employed which comprises a plurality of voltage monitoring units. It is desirable to thermally 30 isolate the sensing thermistors in the voltage monitoring units from the fuel cell stack itself in order to prevent heat generated by

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the stack from interfering with the function of the voltage monitoring units.

The aforementioned voltage monitoring units and cell voltage monitor are useful for 5 monitoring for voltage reversal in fuel cell stacks, especially solid polymer electrolyte fuel cell stacks. Desirably, a low voltage in any fuel cell in the stack may be detected and an appropriate action may then be initiated to 10 prevent damage to the cells.

Brief Description of the Drawings

Figure 1 is a schematic diagram of a solid polymer fuel cell stack in which each pair of 15 cells is equipped with a thermistor-based voltage monitoring unit comprising a reference thermistor.

Figure 2 shows a cell voltage monitor comprising a plurality of voltage monitoring 20 units mounted on a flexible printed circuit board that is suitable for use with a solid polymer fuel cell stack.

Figure 3 is a schematic diagram of a solid polymer fuel cell stack in which each cell is 25 equipped with a thermistor based voltage monitoring unit comprising a PTC fuse.

Detailed Description of Preferred Embodiments

A solid polymer fuel cell stack equipped 30 with a cell voltage monitor for protecting against voltage reversal is shown in the schematic diagram of Figure 1. Fuel cell stack

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1 comprises a stack of eight solid polymer
electrolyte fuel cells in series C₁, C₂, ...,
C₈. Cell voltage monitor 2 employs four voltage
monitoring units (not referenced in Fig. 1),
5 with one unit used for each pair of cells in
stack 1. Each voltage monitoring unit
comprises a heating resistor H_i, a rectifier R_i,
a sensing thermistor ST_i, a reference thermistor
RT_i, and a diode D_i where i represents a voltage
10 monitoring unit number from 1 to 4.

As shown in Figure 1, the voltage of each
pair of fuel cells in stack 1 is monitored by a
corresponding voltage monitoring unit. Current
flows through series-connected heating resistor
15 H_i, and rectifier R_i in accordance with the
voltage across the corresponding pair of fuel
cells C_{2i-1}, C_{2i} and heat is dissipated in
heating resistor H_i. Rectifier R_i is arranged
such that no current flows when the voltage of
20 the pair of fuel cells is negative (implying at
least one cell is in voltage reversal) and, in
this case, no heat is dissipated in heating
resistor H_i.

Each sensing thermistor ST_i is physically
25 located near corresponding heating resistor H_i
and is thermal communication therewith but
electrically isolated therefrom. Additionally,
each sensing thermistor ST_i is located to avoid
contacting other significant sources of heat
30 (for example, stack 1 and/or other heating
resistors). In Figure 1, sensing thermistors
ST_i are connected in series with corresponding

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reference thermistors RT_i . Reference thermistors RT_i are physically located to be at ambient temperature and are not heated significantly by heating resistors H_i . The 5 series-connected sensing thermistors ST_i and reference thermistors RT_i are connected in parallel to reference voltage supply 3. Diodes D_i are connected between common signal line 4 and each series-connected sensing thermistor ST_i 10 and reference thermistor RT_i . During operation of stack 1, the voltage at signal line 4 is monitored using a suitable voltage measuring apparatus.

In the embodiment of Fig. 1, sensing and 15 reference thermistors ST_i , RT_i are preferably of the same type and have negative temperature coefficients. Thus, when heated, the voltage across a sensing thermistor ST_i will be less than that across corresponding reference 20 thermistor RT_i . When not heated, the voltage across a sensing thermistor ST_i will be the same as that across corresponding reference thermistor RT_i (that is, half the voltage provided by reference voltage supply 3). 25 Diodes D_i prevent current from a sensing thermistor at a higher voltage from flowing through other sensing thermistors at lower voltages. Thus, common signal line 4 will indicate the highest voltage of any of the 30 sensing thermistors in voltage monitor 2. The presence of a higher than normal voltage observed at signal line 4 thus warns of at

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least one low voltage pair of cells and appropriate corrective action can be taken to prevent any damage from occurring due to voltage reversal in stack 1.

5 An advantage of this arrangement is that the signal line can provide quantitative information about a cell pair voltage during a low voltage condition. That is, signal line voltages above normal but less than half that
10 provided by reference voltage supply 3 are representative of a cell pair voltage below normal but above zero.

Another advantage of this arrangement is that voltage detection may be largely
15 independent of the ambient temperature around the fuel cell stack. As long as the temperature of each set of sensing and reference thermistors ST_i , RT_i would be similar absent the effect of heating resistors H_i , the
20 ambient temperature around the fuel cell stack can vary without affecting operation of the cell voltage monitor in Figure 1.

In selecting appropriate combinations of components for use in a voltage monitoring
25 unit, the power drained by each heating resistor during normal stack operation should be sufficient for heating its associated sensing thermistor without involving a significant parasitic power drain on the
30 associated fuel cell. It may therefore be preferable to use positive temperature coefficient thermistors as the heating

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- resistors H_i . By so doing, the heating thermistors can generate sufficient heat to activate the sensing thermistors at the lower end of the normal operating voltage range of
5 the cell without generating excessive heat (and hence without draining excessive power) at the higher end of the normal operating voltage range. Further, an appropriate combination of components provides for voltage detection
10 values and response times that allow for normal stack operation without falsely alarming of voltage reversal yet while still providing adequate warning of voltage reversal in abnormal operation situations.
- 15 As an example, a solid polymer electrolyte fuel cell stack might comprise a series stack of cells normally delivering about 50 amps at about 0.6 V (maximum load) and operating at about 1 V at low load. The operating
20 temperature of the stack might typically be in a range from about 60 to 100°C. A thermistor-based cell voltage monitor as described above may be suitable for voltage reversal protection of such a stack. For instance, 9 ohm resistors
25 (0805 package) and I R 10MQ040 type diodes may be used as the heating resistors H_i and rectifiers R_i respectively. The sensing thermistors ST_i and reference thermistors RT_i may be Fenwal 173-103LAF-301 negative
30 temperature coefficient devices. The diodes D_i may be small signal diodes and a 12 volt supply may be used as the reference voltage supply 3.

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In this example, the power dissipated through the heating resistors would be approximately 160 to 440 mW, an acceptable parasitic load. The sensing and reference thermistors are nominally about 10 k Ω but the sensing thermistors will quickly (about 10 seconds) drop and equilibrate to about 5 k Ω or lower when resistively heated at levels more than about 150 mW. Thus, the voltage across the sensing thermistors could be about one third or less that of the reference voltage (that is, less than or equal to about 4 volts) when all the cells are operating normally.

When a cell pair voltage drops to zero or goes negative, the voltage across the associated sensing thermistor and hence also on signal line 4 would be 6 volts. These voltage differences are large enough to discriminate normal from abnormal voltage conditions.

Timeframes of order of 10 seconds represent a reasonable response time for monitoring for voltage reversal in the fuel cell stack, yet brief spikes in the stack output would not affect the signal line value.

A cell voltage monitor 15 suitable for use in such a solid polymer electrolyte fuel cell stack is shown in Figure 2. A plurality of voltage monitoring units (not referenced in Fig. 2) may be surface mounted on flexible printed circuit board 12. Each unit comprises an isothermal package P_i , reference thermistor RT_i , and diode D_i . (Figure 2 shows components

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for the first voltage monitoring unit $i=1$ and
for an arbitrary unit i .) Isothermal package P_i
contains heating resistor H_i , rectifier R_i , and
sensing thermistor ST_i which are coated with a
5 thermosetting polymer (such as Glob-top
thermoset ME-410). Conductive traces
electrically connect components in the voltage
monitoring units to fuel cell contacts 14.
Cell voltage monitor 15 is mounted to the edge
10 of the fuel cell stack (not shown) by clamping
or using a conductive glue such that fuel cell
contacts 14 are electrically-connected
appropriately to the fuel cells in the stack.
The portions of printed circuit board 12
15 comprising packages P_i , reference thermistors
 RT_i , and diodes D_i would not contact the fuel
cell stack in order to thermally isolate them
from heat generated by the stack itself. Figure
2 also shows wire connections to the printed
20 circuit board 12 for signal line 16 and
reference voltage supply leads 17, 18.

The preceding example describes a possible
combination of components and packaging
suitable for monitoring pairs of cells to
25 prevent voltage reversals in a certain type and
size of fuel cell stack. However, such cell
voltage monitors and/or voltage monitoring
units may be useful for other purposes in solid
polymer electrolyte or other types of fuel
30 cells. It may be desirable to adapt the
voltage monitoring units for purposes of
monitoring individual cells. Further,

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alternative detection circuits may be considered that do not require reference thermistors or negative coefficient sensing thermistors. For instance, another possible 5 embodiment is shown in Figure 3, which employs PTC fuses as the sensing thermistors.

Figure 3 is a schematic diagram of a solid polymer fuel cell stack in which each cell is equipped with a thermistor-based voltage 10 monitoring unit comprising a PTC fuse. Fuel cell stack 21 comprises a stack of n solid polymer electrolyte fuel cells in series C₁, C₂, ..., C_n. Cell voltage monitor 22 comprises n corresponding voltage monitoring units U₁, U₂, 15 ..., U_n. Each voltage monitoring unit U_j (where j is a number from 1 to n) comprises a heating resistor H_j, a rectifier R_j, and a PTC sensing thermistor S_j. PTC sensing thermistors S_j are connected in parallel to leads 23, 24. When 20 the voltage of each fuel cell C_j is in a normal operating range, thermistors S_j are heated by heating resistors H_j such that they exhibit high resistance (that is, open). However, when a fuel cell drops to too low a voltage, the 25 associated PTC sensing thermistor cools and drops markedly in resistance (that is, closed). Thus, a simple continuity check at leads 23, 24 provides an indication of a low voltage cell.

While particular elements, embodiments and 30 applications of the present invention have been shown and described, it will be understood, of course, that the invention is not limited

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thereto since modifications may be made by
those skilled in the art without departing from
the scope of the present disclosure,
particularly in light of the foregoing
5 teachings.

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What is claimed is:

1. A voltage monitoring unit for monitoring the voltage of at least one cell in a fuel cell stack, the unit comprising:
 - 5 a heating resistor;
 - a rectifier in series with said heating resistor; and
 - 10 a sensing thermistor, said sensing thermistor being electrically isolated from and in thermal communication with said heating resistor.
2. The voltage monitoring unit of claim 1 additionally comprising a reference thermistor in series with said sensing thermistor and thermally isolated from said heating resistor.
- 20 3. The voltage monitoring unit of claim 2 wherein said reference thermistor and said sensing thermistor have the same resistance as a function of temperature characteristics.
- 25 4. The voltage monitoring unit of claim 2 additionally comprising a diode electrically-connected at one end between said series-connected sensing and reference thermistors.
- 30 5. The voltage monitoring unit of claim 1 wherein the resistance of said sensing

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thermistor changes substantially with an increase in temperature above ambient.

6. The voltage monitoring unit of claim
5 5 wherein said sensing thermistor is a
resettable thermal switch.

7. The voltage monitoring unit of claim
6 6 wherein said sensing thermistor is a
10 polymeric positive temperature coefficient
fuse.

8. The voltage monitoring unit of claim
1 1 wherein said heating resistor is a positive
15 temperature coefficient thermistor.

9. The voltage monitoring unit of claim
1 1 wherein said heating resistor, said rectifier
and said sensing thermistor are each coated
20 with a thermosetting polymer.

10. A cell voltage monitor for a fuel
cell stack comprising a plurality of the
voltage monitoring units of claim 1.
25

11. The cell voltage monitor of claim 10
wherein the series-connected heating resistors
and rectifiers in each of said plurality of
voltage monitoring units are connected in
30 series.

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12. A cell voltage monitor for a fuel cell stack comprising a plurality of the voltage monitoring units of claim 2.

5 13. The cell voltage monitor of claim 12 wherein the series-connected reference thermistors and sensing thermistors in each of said plurality of voltage monitoring units are connected in parallel across a reference
10 voltage supply.

14. A cell voltage monitor for a fuel cell stack comprising a plurality of the voltage monitoring units of claim 4.

15 15. The cell voltage monitor of claim 14 wherein the series-connected reference thermistors and sensing thermistors in each of said plurality of voltage monitoring units are connected in parallel across a reference voltage supply, and the other ends of the diodes in each of said plurality of voltage monitoring units are connected to a common signal line.
20

25 16. The cell voltage monitor of claim 15 wherein the polarity of said diodes is such that current is prevented from flowing from an unheated one of said sensing thermistors to a heated one of said sensing thermistors via said common signal line.
30

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17. A cell voltage monitor for a fuel cell stack comprising a plurality of the voltage monitoring units of claim 6.

5 18. The cell voltage monitor of claim 17 wherein the resettable thermal switches in each of said plurality of voltage monitoring units are connected in parallel.

10 19. The cell voltage monitor of claim 10 wherein said plurality of voltage monitoring units are mounted on a flexible printed circuit board.

15 20. A fuel cell stack comprising the voltage monitoring unit of claim 1 wherein the series-connected heating resistor and rectifier in said voltage monitoring unit are electrically-connected across at least one fuel cell in said fuel cell stack.

20 21. The fuel cell stack of claim 20 wherein the polarity of said rectifier is such that current is prevented from flowing through said series-connected resistor and rectifier when said fuel cell is in voltage reversal.

25 22. The fuel cell stack of claim 20 wherein said stack comprises a plurality of series-connected fuel cells and a cell voltage monitor comprising a plurality of voltage monitoring units.

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23. The fuel cell stack of claim 22
wherein each of said voltage monitoring units
is connected across a pair of said fuel cells
5 in said stack.

24. The fuel cell stack of claim 20
wherein the fuel cells in said stack are solid
polymer electrolyte fuel cells.

10 25. A method for detecting a low voltage
in a fuel cell in a fuel cell stack comprising:
 connecting a heating resistor and a
15 rectifier in series across said fuel cell
 wherein the polarity of said rectifier is
 such that current is prevented from
 flowing through said rectifier when said
 fuel cell is in voltage reversal;
 positioning a sensing thermistor in
20 thermal communication with and
 electrically isolated from said heating
 resistor such that said sensing thermistor
 is heated when current flows through said
 heating resistor; and
25 obtaining a signal indicative of the
 resistance of said sensing thermistor.

26. The method of claim 25 wherein said
signal is obtained by:
30 connecting a reference thermistor in
 series with and thermally isolated from
 said sensing thermistor;

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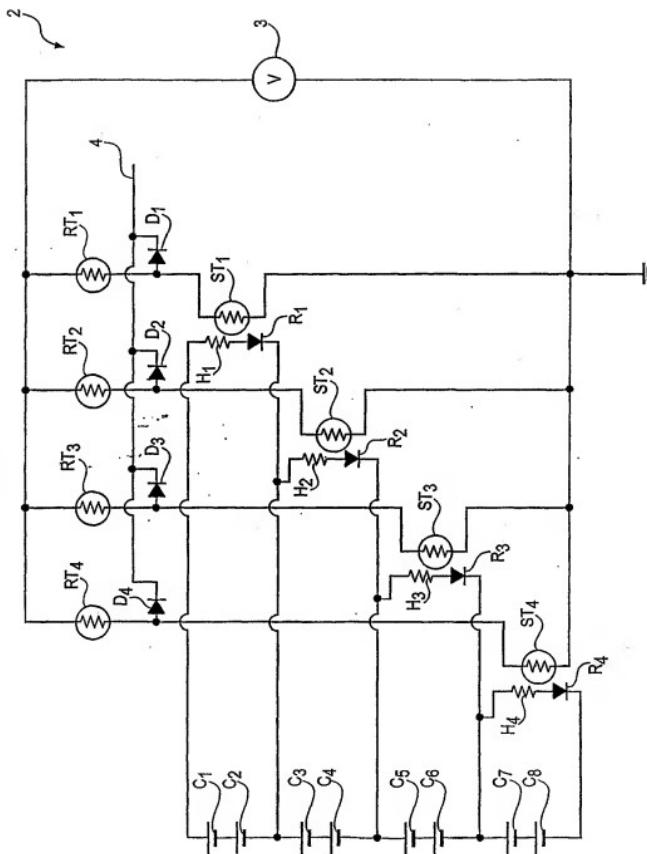
applying a reference voltage across
the series-connected sensing and reference
thermistors; and
measuring the voltage across said
sensing thermistor.

5 27. The method of claim 25 wherein said
sensing thermistor is a resettable thermal
switch and said signal indicates whether said
10 resettable thermal switch is open or closed.

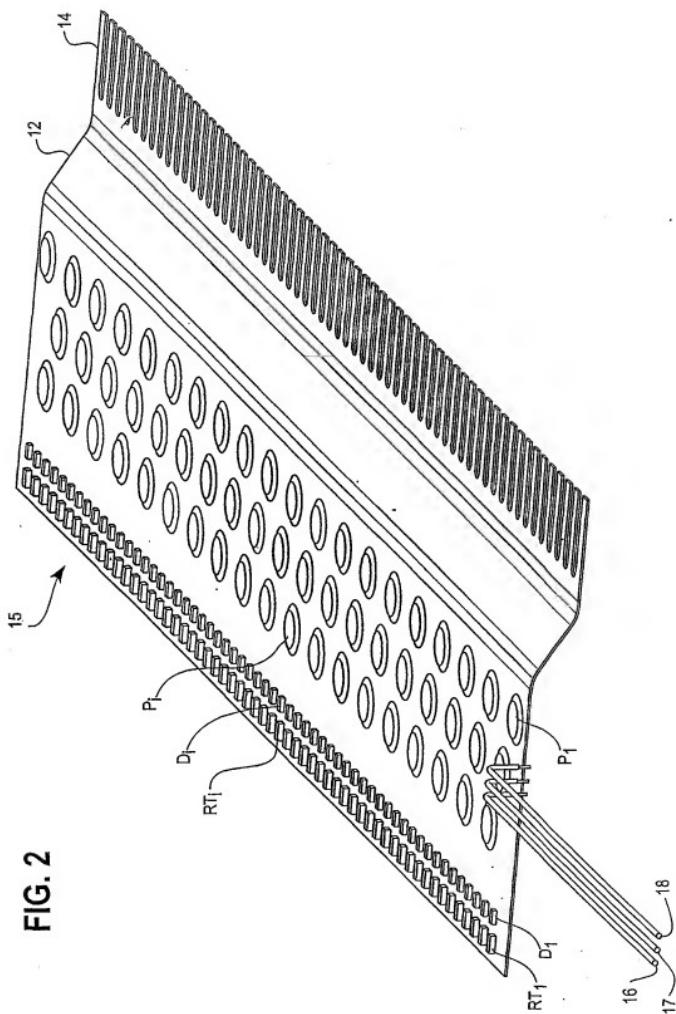
15 28. The method of claim 25 comprising
thermally isolating said sensing thermistor
from said fuel cell stack.

20 29. A method of monitoring for voltage
reversal in a fuel cell stack comprising using
the method of claim 25 to detect for any low
voltage fuel cell in said fuel cell stack.

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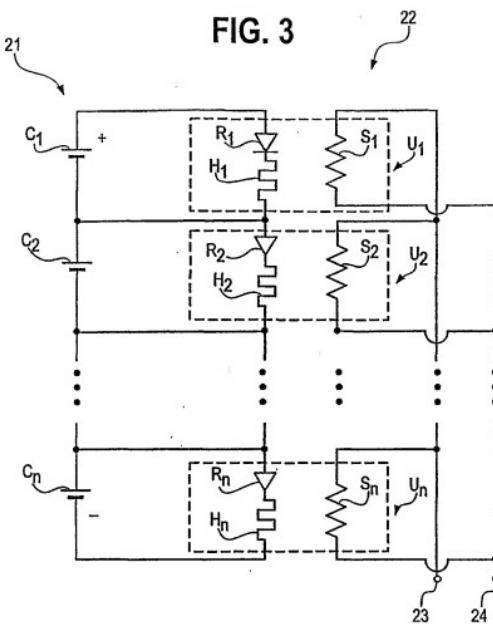
FIG. 1

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3/3

FIG. 3



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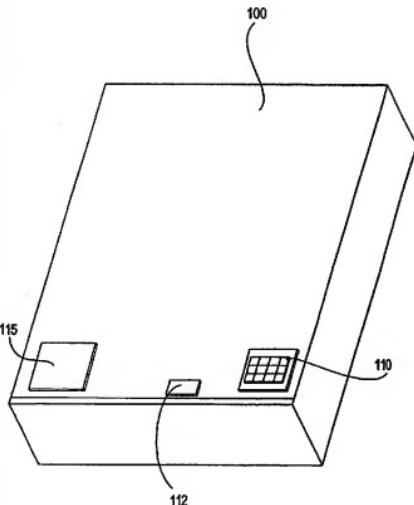
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{Continued on next page}

(54) Title: METHOD AND APPARATUS FOR A HYDROGEN FUEL CASSETTE DISTRIBUTION AND RECOVERY SYSTEM

WO 2003/078252 A3



(57) Abstract: A cassette-based hydrogen fuel distribution and recovery system comprising a cassette (100) including a conventional electronic device (110) to store and process information related to the cassette and a memory and telemetry device (115) for communicating back cassette information to a control software system.



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International application No.
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A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) : C10J 3/20
US CL : 48/18.5, 197R, 61; 423/648.1, 658.2; 252/373

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
U.S. : 48/18.5, 197R, 61, 423/648.1, 658.2; 252/373

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 3,977,990 A (BECKERT et al.) 31 August 1976 (31.08.1976)	1-20
A	US 3,932,600 A (GUTBIER et al.) 13 January 1976 (13.01.1976)	1-20
A	US 3,674,702 A (MACKENZIE et al.) 04 July 1972 (04.07.1972)	1-20

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